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sonable motor efficiency ξ_M. Likewise, jet aircraft compressors have efficiencies of 85% to 90% or better. Thus, one expects a conservative compressor efficiency ξ_C of 85%. The combined overall system efficiency should be equal to or greater than the following:

67. PAGE 32, LINE 19:

The power costs required for the processes of the present invention can be computed by noting that the primary power source is the compressor shaft power. The system also requires an additional small amount of energy for rotational acceleration of the fluid in the boiler/condenser shells. Applicants estimate that additional energy to be approximately 0.2 W hrs/lb for the exemplary 350 gallon/day system.

68. PAGE 33, LINE 1:

One acre-foot = 1.23 x 10^6 liters. In this expression E_ρ^{ξ} is the system specific energy (FIG. 22) in Watt-hours per pound and $C_{¢}$ is the cost of electrical power that the utility charges in cents per kilowatt-hour.

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69. PAGE ~~34~~ 33, LINE ~~26~~ 22:

The general relation that describes the boiling heat transfer coefficient in both the pool and nucleate boiling regimes is based on work by Rohsenow (*See*, for instance, *Handbook of Applied Thermal Design*, Eric C. Guyer, Editor in Chief, McGraw Hill 1989, pp. 1-79). Guyer references the original work of Rohsenow performed in 1952 using correlated experimental data. The relation developed by Rohsenow has the following general form:

70. PAGE 34, LINE 26:

Results of Boiling Heat Transfer Calculations: Figures 19-24 show a series of computations of the general trends, which occur with rotational g's on boiling heat transfer rates. These figures are both three-dimensional surface renditions and two-dimensional slice plots for two different boiler surface material conditions and three different ambient input temperatures. Some of the figures show the enhanced boiler heat transfer behavior with increased rotational g for a roughly coated Teflon®